



Esempi di modellistica applicata agli slush flows

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Torino, 20 novembre 2025





Cos'è uno slush flow

- Uno slush flow può essere considerato un caso estremo di valanga radente di neve bagnata → presenta pertanto alcune caratteristiche analoghe a tale tipologia di valanghe (capacità di propagarsi anche su pendenze modeste, velocità più contenute dei fenomeni con neve asciutta)
- La caratteristica principale, accanto al moto di tipo radente, è l'elevata concentrazione volumetrica di acqua liquida ($C_w \gg 15\%$), da cui deriva l'elevata densità dell'ammasso in movimento
- Sono fenomeni maggiormente frequenti alle latitudini Nord (artico) rispetto agli ambiti alpini (Norvegia, Islanda, Russia – Penisola di Kola, USA – Alaska)





Slushflow hazard — where, why and when? 25 years of experience with slushflow consulting and research

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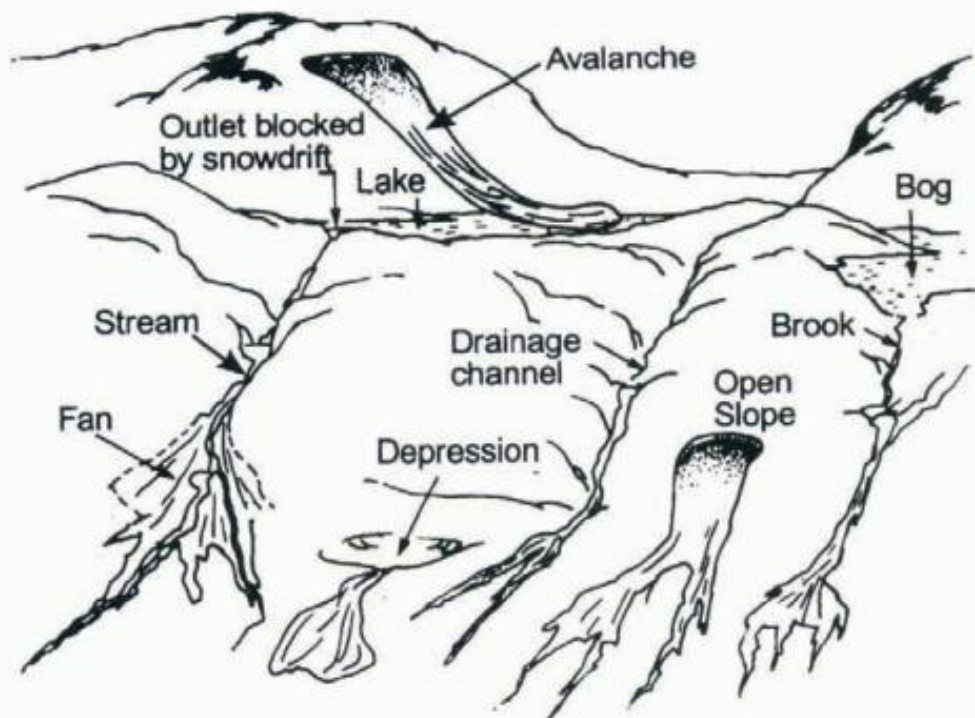
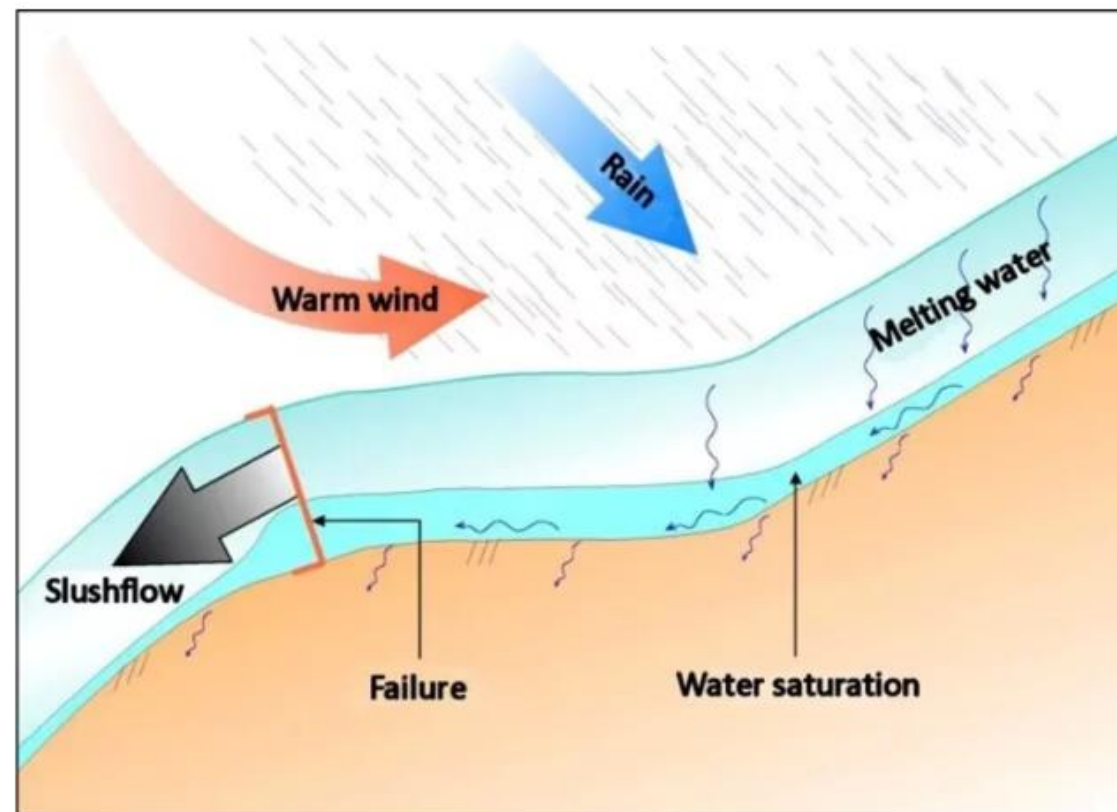


Fig. 7. Starting zones of slushflows.

La differenza più significativa rispetto alle valanghe di neve è la possibilità degli SF di originarsi anche su pendii a ridotta pendenza ($\ll 28\text{-}30^\circ$ deg, fino a $5\text{-}10^\circ$ deg)





A regional early warning for slushflow hazard

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Received: 13 June 2023 – Discussion started: 18 July 2023

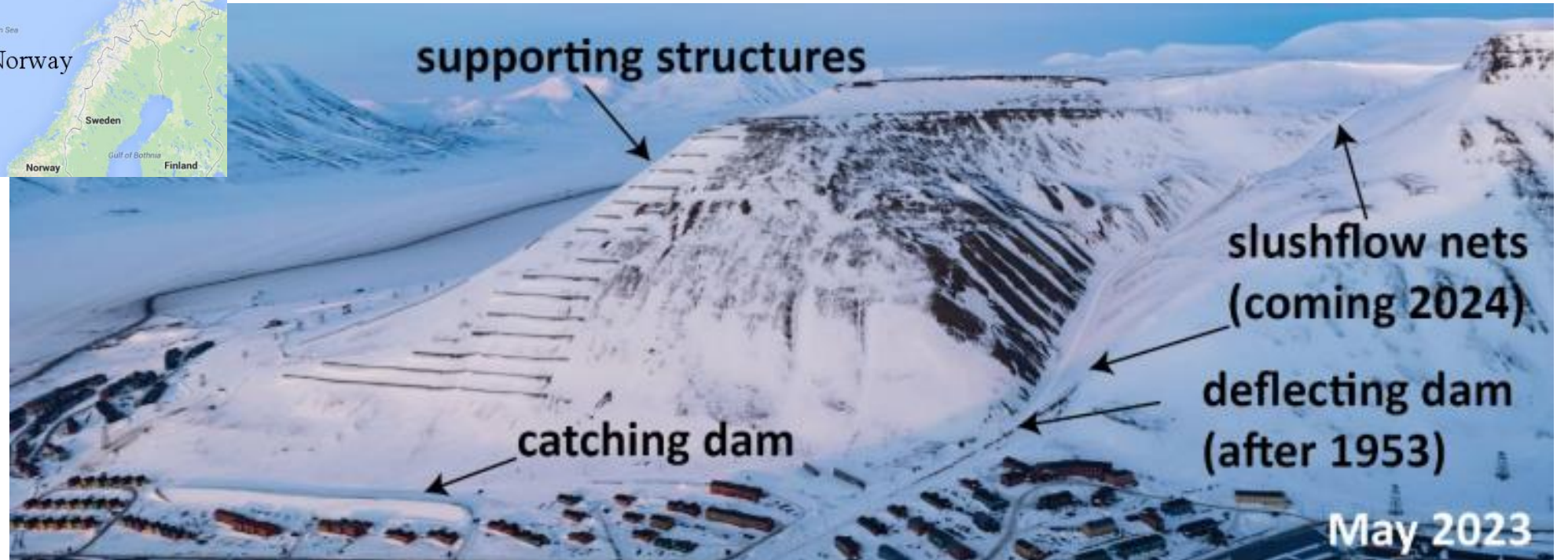
Revised: 22 January 2024 – Accepted: 8 February 2024 – Published: 3 April 2024

ESEMPIO DI SLUSH FLOW PATH & OCCURRENCE



Figure 1. Example of a slushflow path and runout, close to Krossbu, Jotunheimen, southern Norway, 19 May 2013. It released at the outlet of a lake and eroded the ground. It is not uncommon that slushflows initiate in sunny weather due to snowmelt only. (Photo credit: Kjell Nyøygard.)

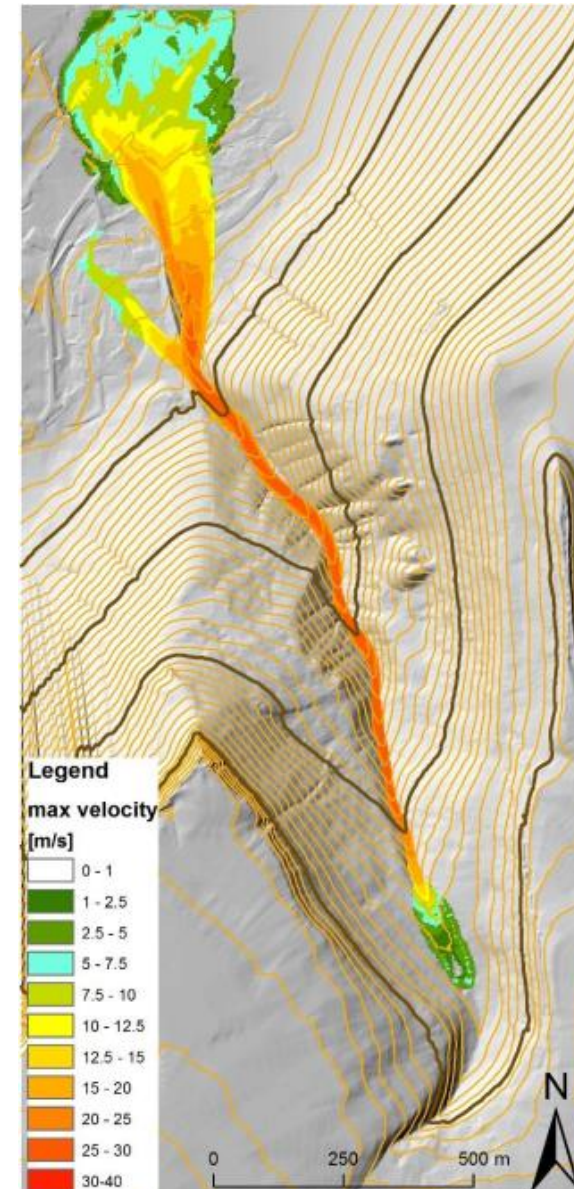
SLUSH HAZARD AT LONGYEARBYEN, SVALBARD



Optimizing Mitigation Measures against Slush Flows by Means of Numerical Modelling-A Case Study Longyearbyen , Svalbard

P. Gauer • Published 2014 • Environmental Science, Engineering

Spitsbergen is usually related to cold climate and harsh weather conditions. In recent years, mild weather in mid-winter has become more frequent, and likewise have slushflows. The latest slushflow incident occurred in Vannledningsdalen January 2012. Longyearbyen Community Council asked NGI for a review of existing mitigation measures, and for a proposal of a revision or extension to fulfill new building regulations. The RAMMS model from SLF/WSL was chosen to simulate the slushflow. The slushflow was first simulated for the existing terrain and input parameters were optimized by comparison with selected known slushflows events. We found the parameters $\mu=0.05$ and $\lambda=5000$ [m/s²] to give reasonable run-out. These parameters were then used in simulations with a modified terrain including the revised mitigation measures. We consider that the use of RAMMS gives valuable indication on how the slushflow might behave along the path, what flow thickness and speed can be expected as well as to indicate possible deficiencies in the proposed design of the mitigation measures. [Collapse](#)



THE DESIGN AND CONSTRUCTION OF SLUSH-FLOW NETS IN VANNLEDNINGSDALEN LONGYEARBYEN SVALBARD

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Figure 7 shows installation of 7 m high posts at net 13 on 19th of August 2024. The horizontal ropes and retaining ropes are connected to the Flexheads/anchors but the work on the ring net is still under way. The photo also shows how fractured and loose the Svalbard rock and soil is. Photo: Arni Jonsson.

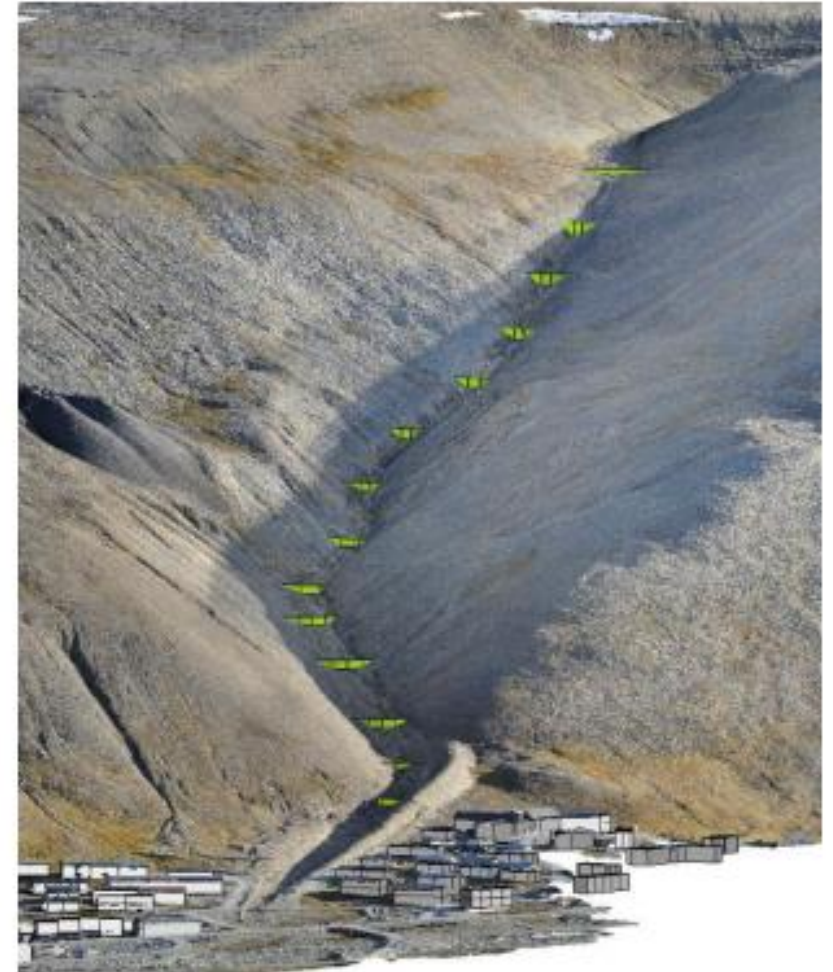
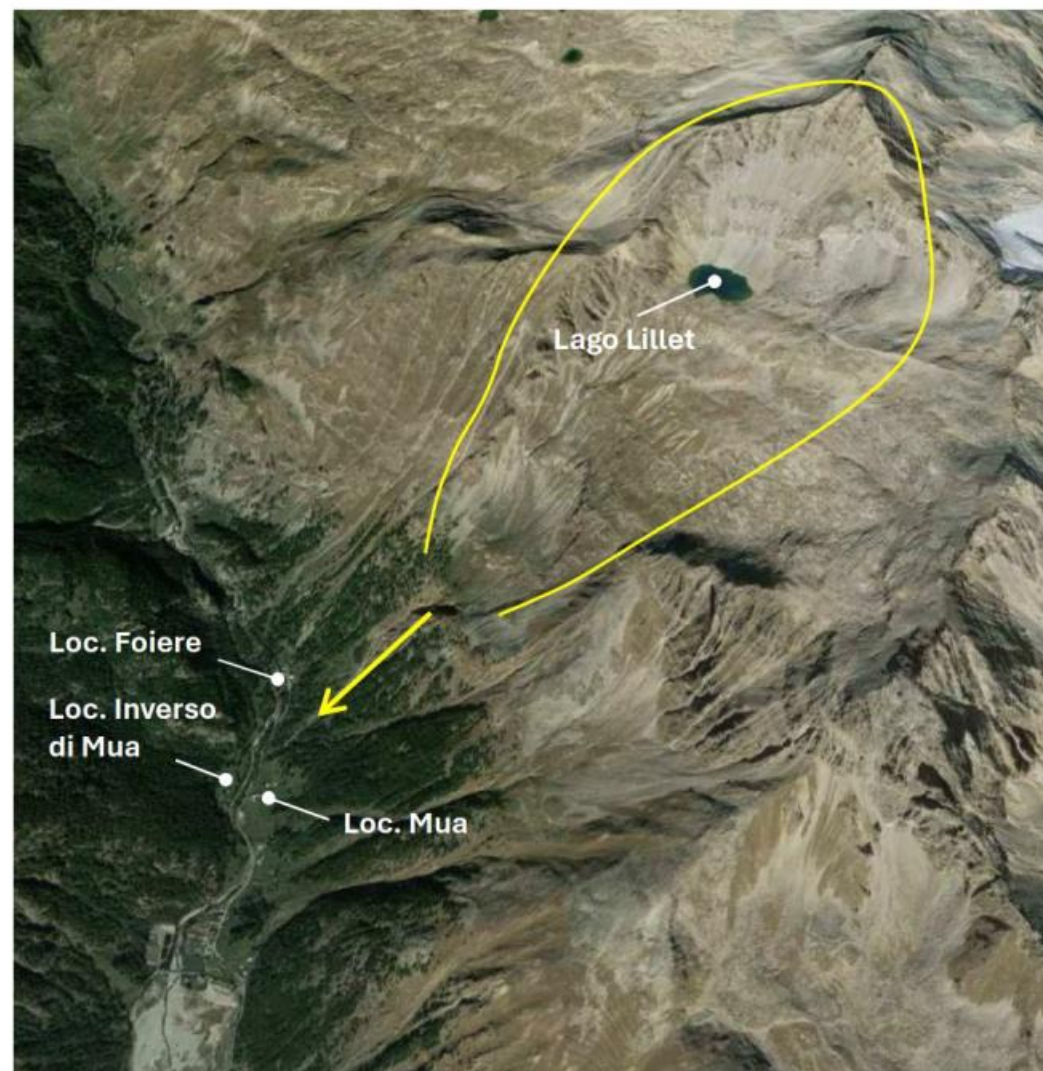
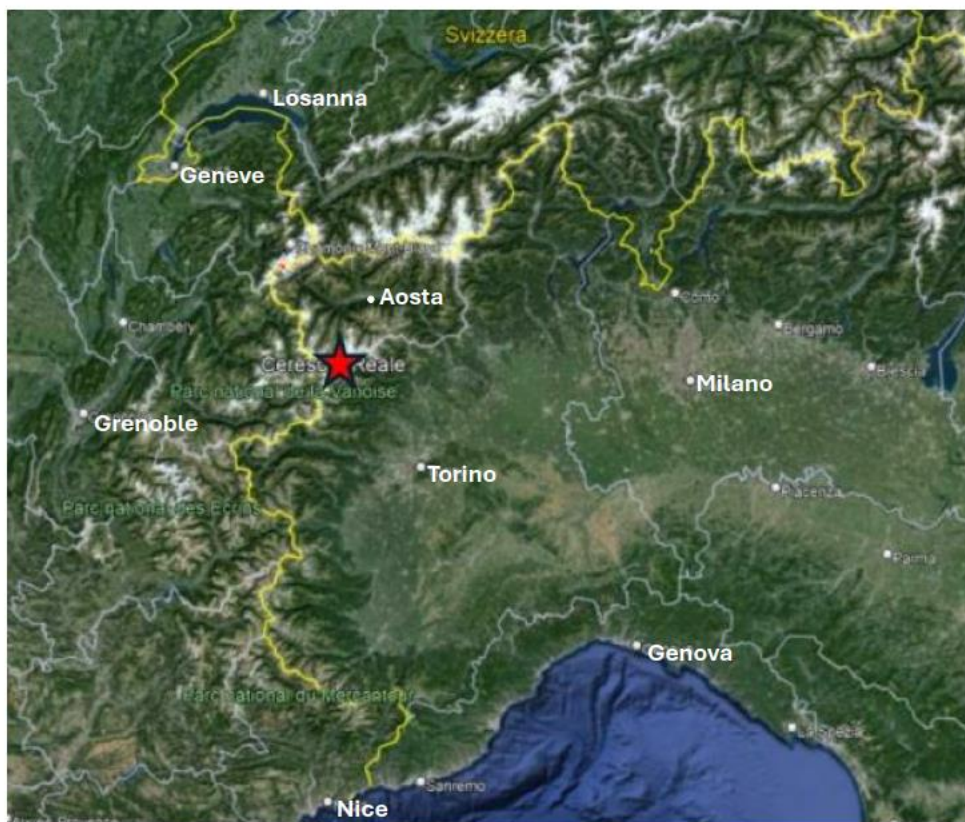


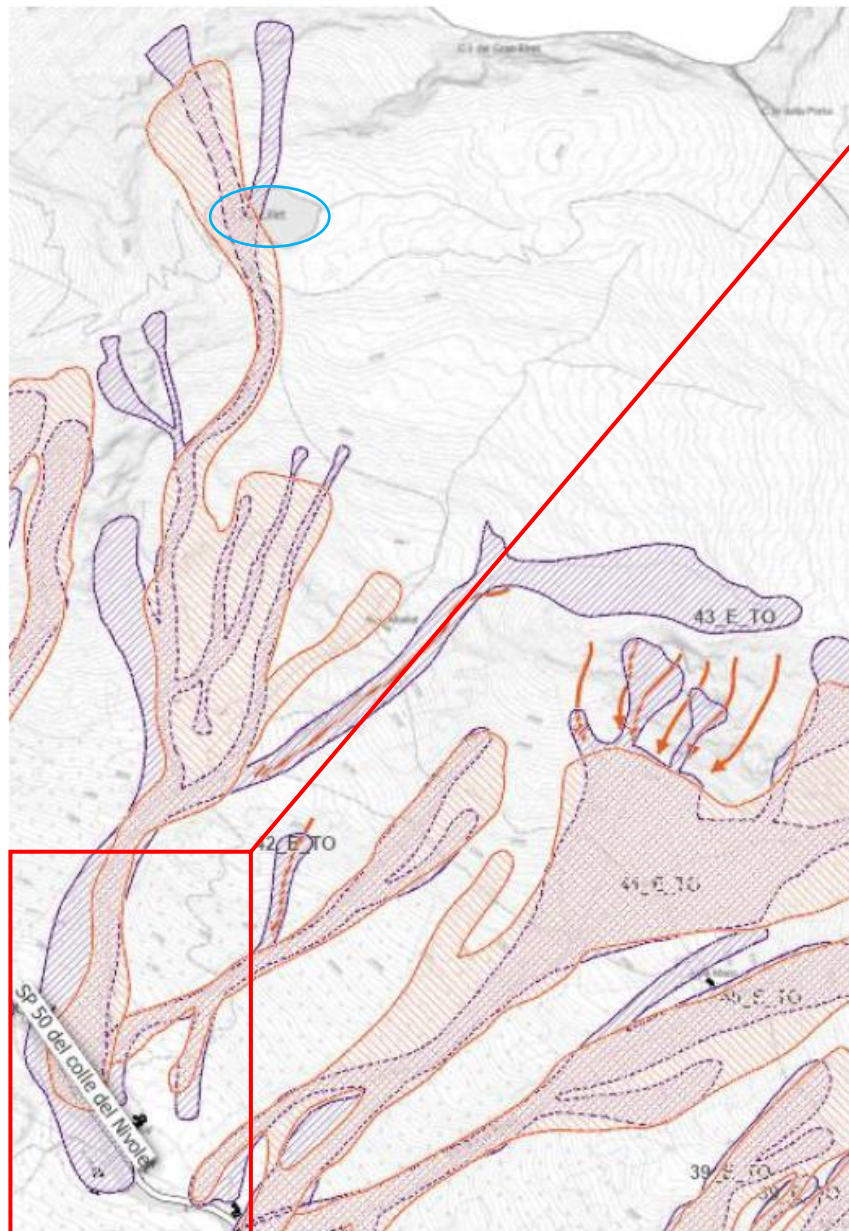
Figure 1 shows Vannledningsdalen and the planned sites for 14 slush-flow nets (highlighted in yellow-green) overlaid on a 3D point cloud model. Fig.: HNIT Verkfræðistofa.

La valanga “Lago Lillet”

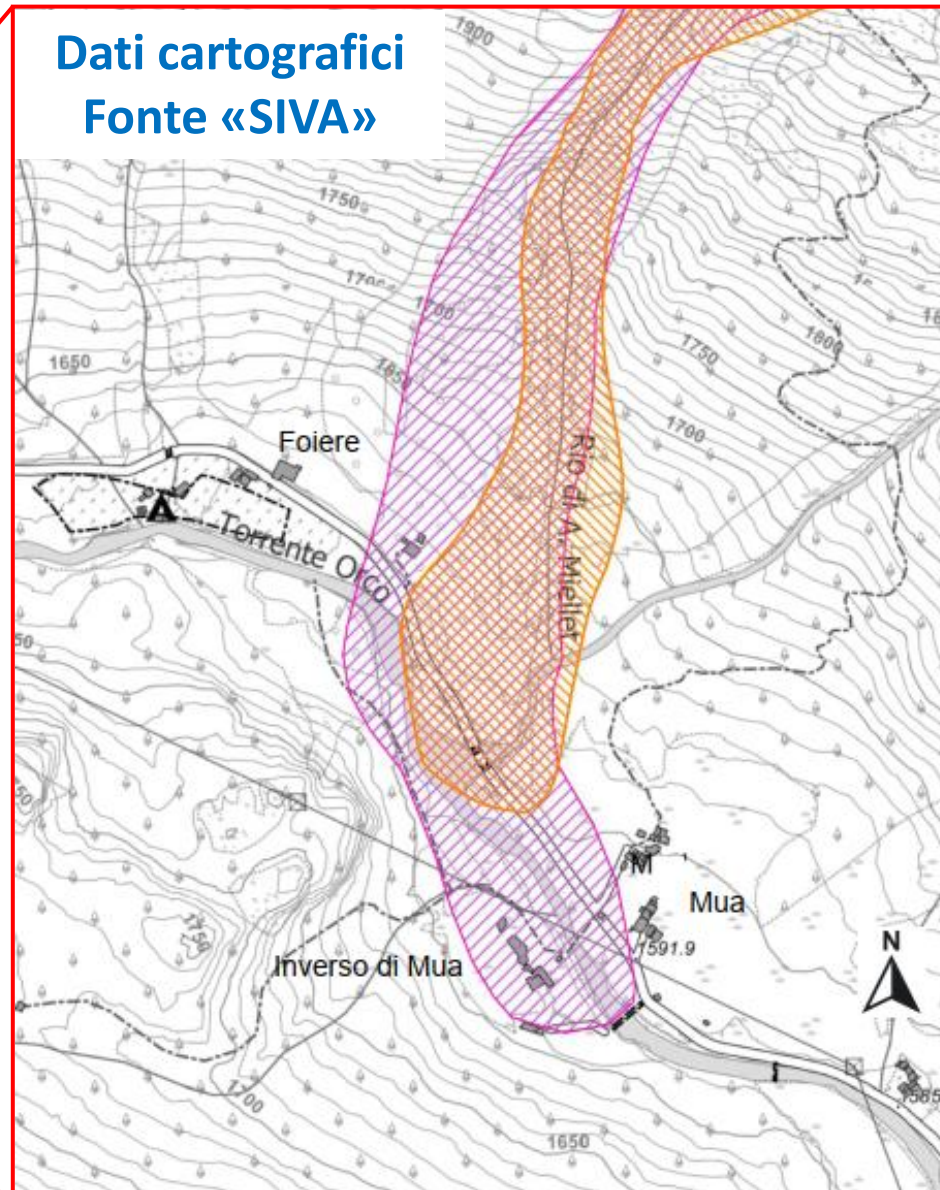
Comune di Ceresole Reale (TO)

n. 43-E-TO del SIVA





Dati cartografici Fonte «SIVA»



Dati Storico-archivistici

SIVA:

“Nel 1972 una parte cadde nel lago Lillet, causandone lo straripamento, giunta a valle distrusse una casa ad Inverso di Mua”

Archivio “Capello”:

“Un ramo cadde nel lago rompendo lo strato di ghiaccio, provocandone lo straripamento, poi si incanalò nel Rio Pisson roccioso e poi boscoso. Superò la strada e si depositò in parte nell’Orco ed in parte presso Foiera”

Dati Storico-archivistici

SIVA

CAPELLO

32. VALANGA DEL LAGO LILLET.

Località. - Si staccò sul fianco sinistro dell'Orco, in vicinanza di Foiera. Tavv. 41 III NE (Colle del Nivolet) e 41 II NO (Ceresole).

Descrizione sommaria. - Scese da un costone roccioso del versante SO del M. Percia, roccioni ad O, presso il lago Lillet. Un ramo cadde nel lago rompendo lo strato di ghiaccio, provocandone lo straripamento, poi si incanalò nel rio Pisson roccioso e poi boscoso. Superò la strada e si depositò in parte nell'Orco ed in parte presso Foiera. Esposizione S. *Dati metrici* - Nel 1972: traiettoria m 2100, fronte m 150, superficie mq 35.000 (C. Forestale).

Periodicità - Durata - Effetti. - Periodica irregolare. Cade solo ogni 15-20 anni. Osservata il 20-2-1972 (ore 10). La neve durò sino ad aprile e lasciò residui detritici, tronchi e ceppaie. Scorticò i pascoli. Asportò linee elettriche per 250 m. Ostruì la strada per il Colle Nivolet.

Fonti delle notizie. - C. Forestale (Locana) - Bazzarone (informaz.).

Cartografia. - Atlante, tavole n. 3 (Nivolet) e n. 4 (Ceresole).



SIVA: SISTEMA INFORMATIVO VALANGHE Scheda di Caratterizzazione del Sito Valanghivo

sito Lago Lillet - località Mua, Ceresole Reale (TO)

Bacino Idrografico:	Orco	Sezione CTR:	112110
Quota massima di distacco (m s.l.m.):	3200	Quota minima di arresto (m s.l.m.):	1600
Dislivello (m):	1600	Lunghezza reale (m):	2600
Sito valanghivo n°	43_E_TO	Sito ASTV	32_4
Tavola cartografica	Valle Orco: Ceresole Reale, Noasca	Tavola ASTV	Ceresole Reale
Modalità di acquisizione	Terreno e archivio	Frequenza	Periodica (ogni 2-30 anni)

ZONA DI DISTACCO	ZONA DI SCORRIMENTO
Ubicazione	Profilo
Morfologia	Andamento planimetrico
Inclinazione media	Morfologia
Esposizione media	Inclinazione media
Substrato	Substrato

ZONA DI ARRESTO	OPERE DI DIFESA
Luogo di arresto	Tipologia
Note	Note

DANNI POTENZIALI	DANNI ACCERTATI

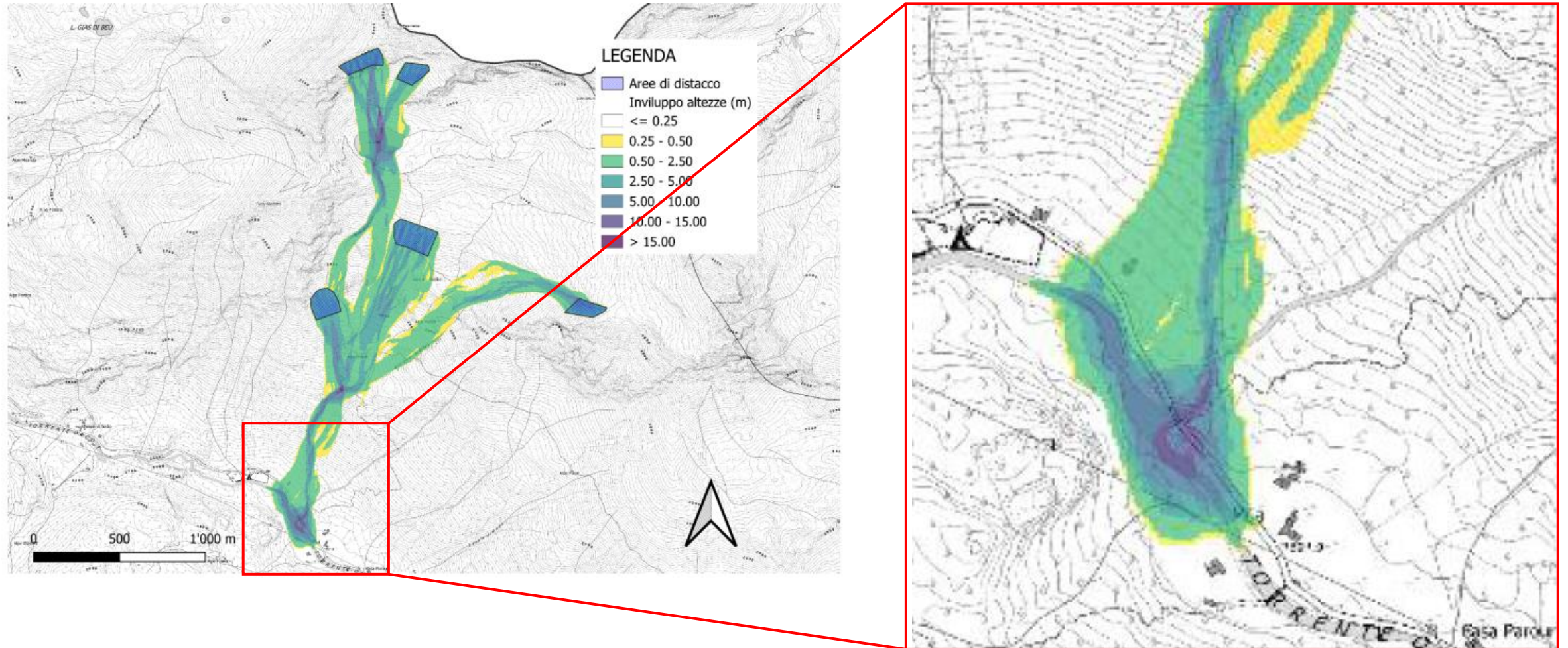
EVENTI NOTI	INFORMAZIONI AGGIUNTIVE
1972 febbraio 20	Mod.7 Aineva
2008 dicembre 16	Note generali

FOTO	FONTI
Non presenti	Non presenti
Rilevatore	Data primo rilevamento
Autore aggiornamento	Data aggiornamento

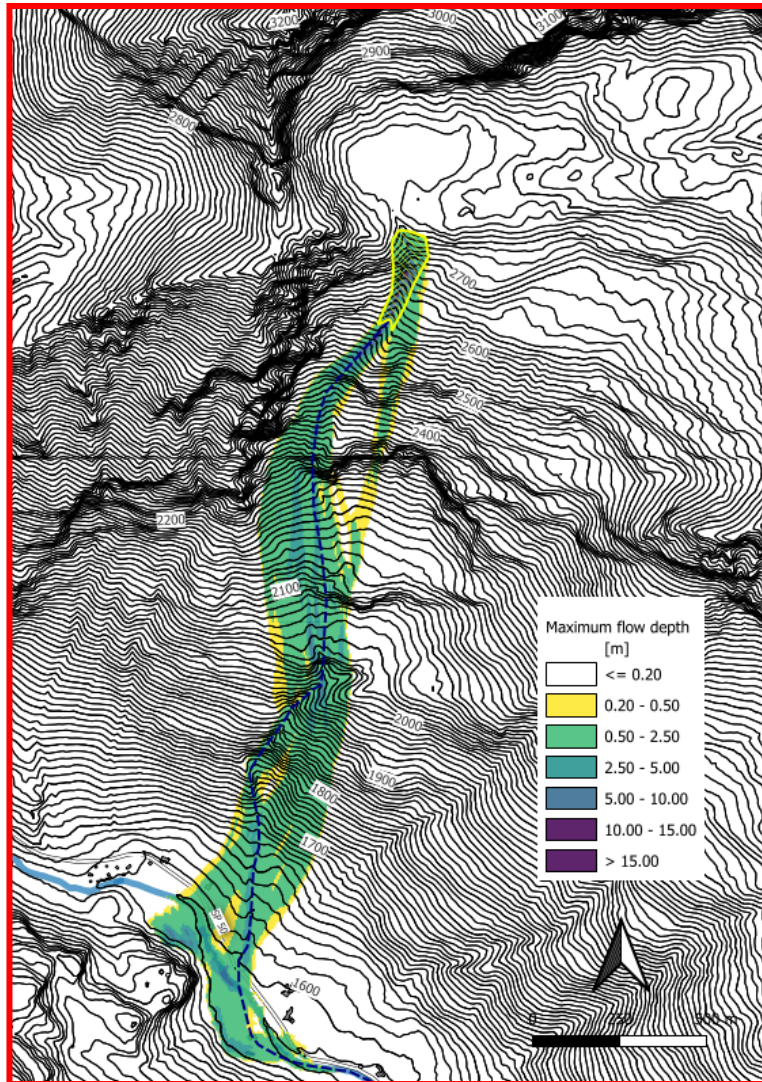
Nel 1972 una parte cadde nel lago Lillet, causandone lo straripamento, giunta a valle distrusse una casa ad Inverso di Mua.

Evento valanghivi di tipo denso a carattere eccezionale – T=300 anni

Modello – RAMMS::Avalanche



MODELLAZIONE EVENTO TIPO SLUSH-FLOW



**Modello – RAMMS::Avalanche
con parametrizzazione «ad hoc»**

$$\mu=0.05$$
$$\xi=5000 \text{ (m/s}^2\text{)}$$

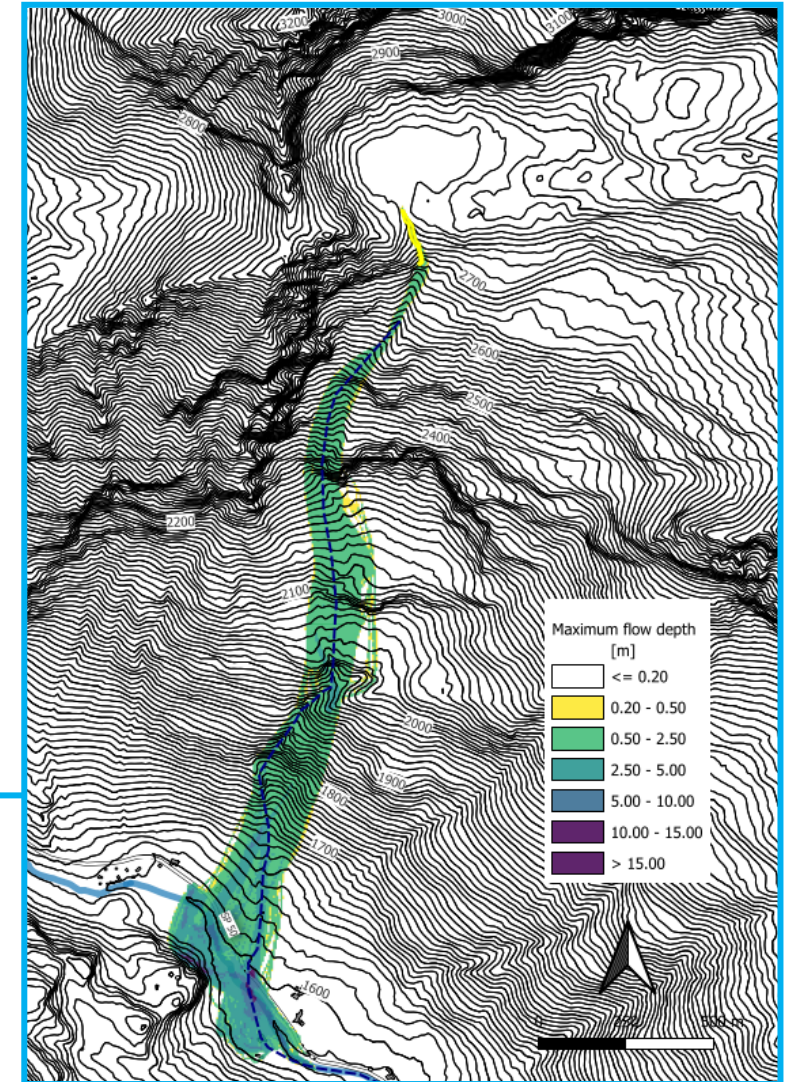
(Rif. Jónsson and Gauer, 2014)

Modello – SAMOS-AT Modified

$$(\sigma_{xz}, \sigma_{yz}) = \frac{u}{\|u\|} \left[3M_B \frac{\|u\|}{h} + 1,5 \tau_y + \mu \sigma_{zz} \right]$$

Coulomb friction $\mu=0.1$
Shear strength $\tau_y=100\text{Pa}$
Bingham viscosity $M_B=5 \text{ Pa}\cdot\text{s}$
Max. erodible mass: 300 kg/m^2

(Rif. Barbolini et al., 2024)



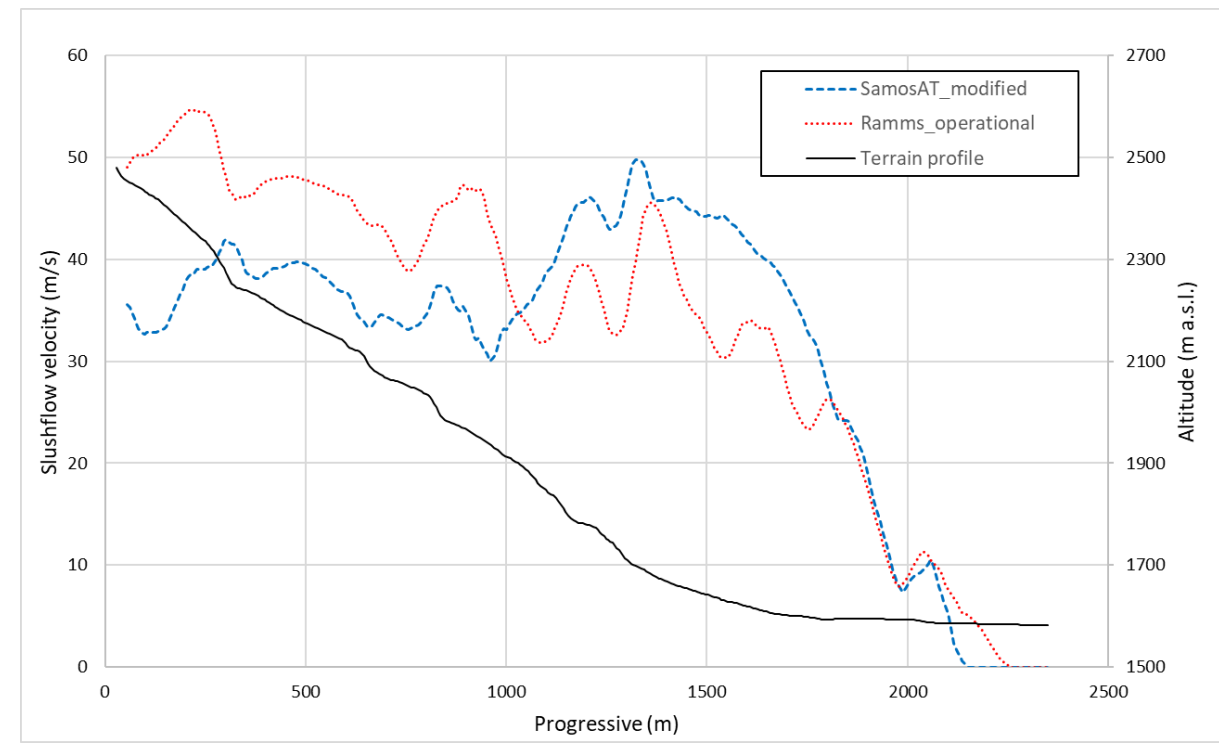
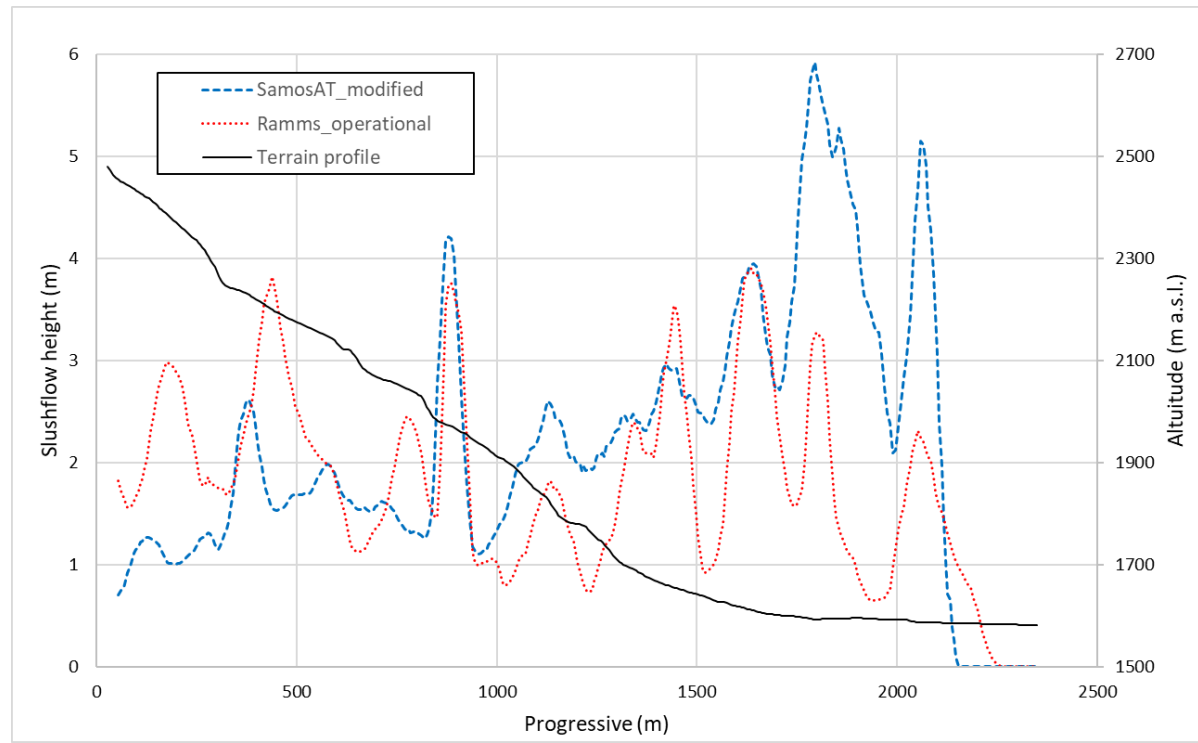
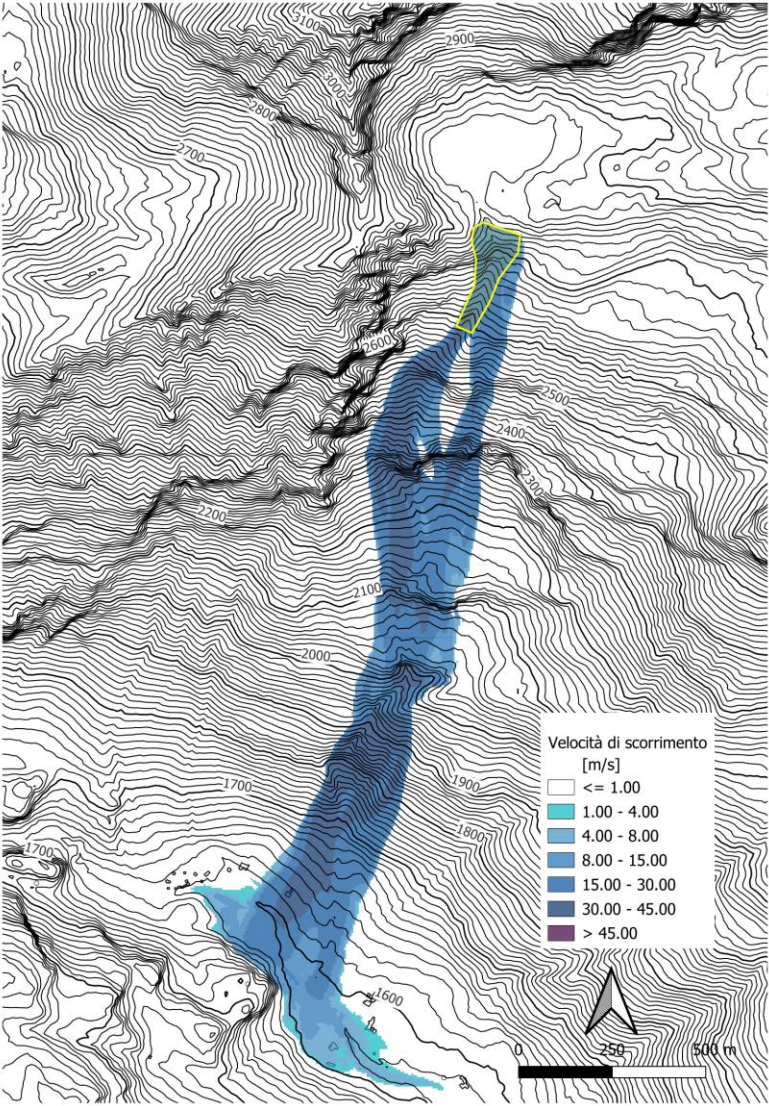
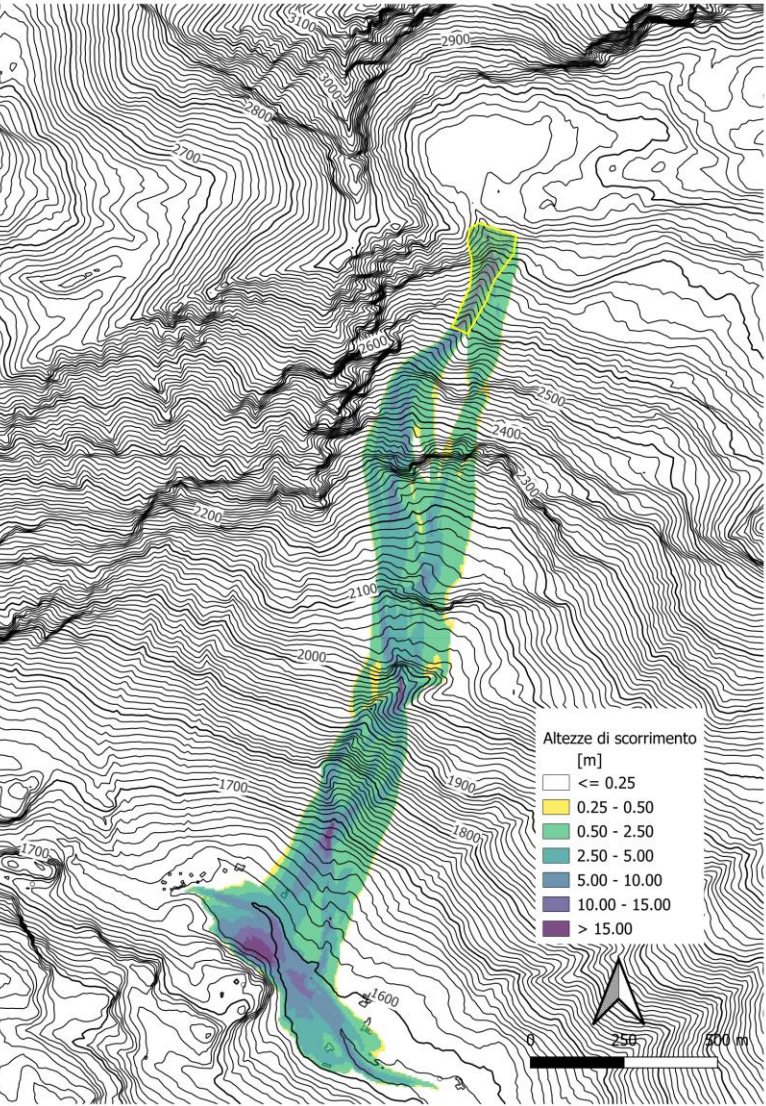


Figure 6: Comparison of slushflow simulation: maximum flow heights obtained with Ramms::operational (top-left) and Samos-AT (top-right). Lower pictures show the comparison of calculated slushflow height and velocity along the green profile of Figure 5, indicated with a dashed line in the top figures.

MODELLAZIONE EVENTO TIPO SLUSH-FLOW

Modello – RAMMS::Extended



EXTENDED	DTM UTILIZZATO	RIS	AREA DI DISTACCO	V
Nome file		m	Nome shapefile	mc
SIM_SLUSHFLOW_EXT_07	DTM_5M_EPSG32633	5	CERESOLE REALE release area slushfl gw	72'336.8

TEMPO DI RITORNO	HD	COES.	AVAL. DIM	DUMP STEPS	END TIME
anni	m	Pa		s	
300	2.5	0	LARGE	5	500

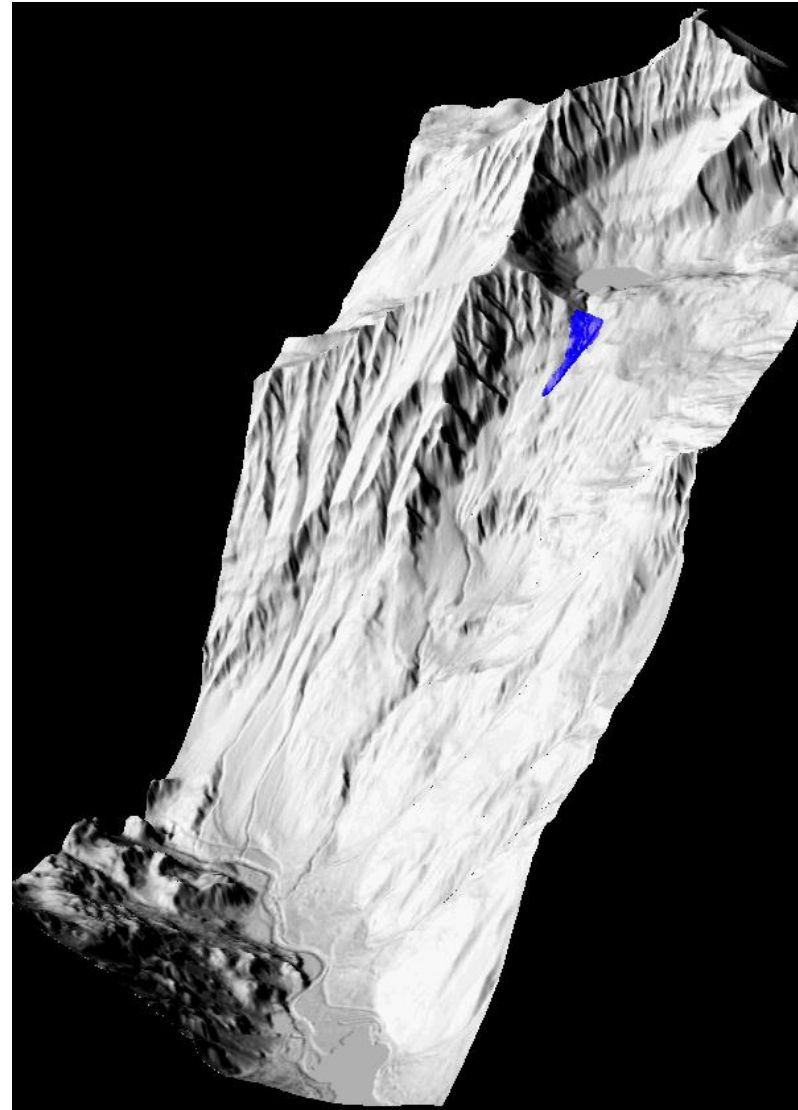
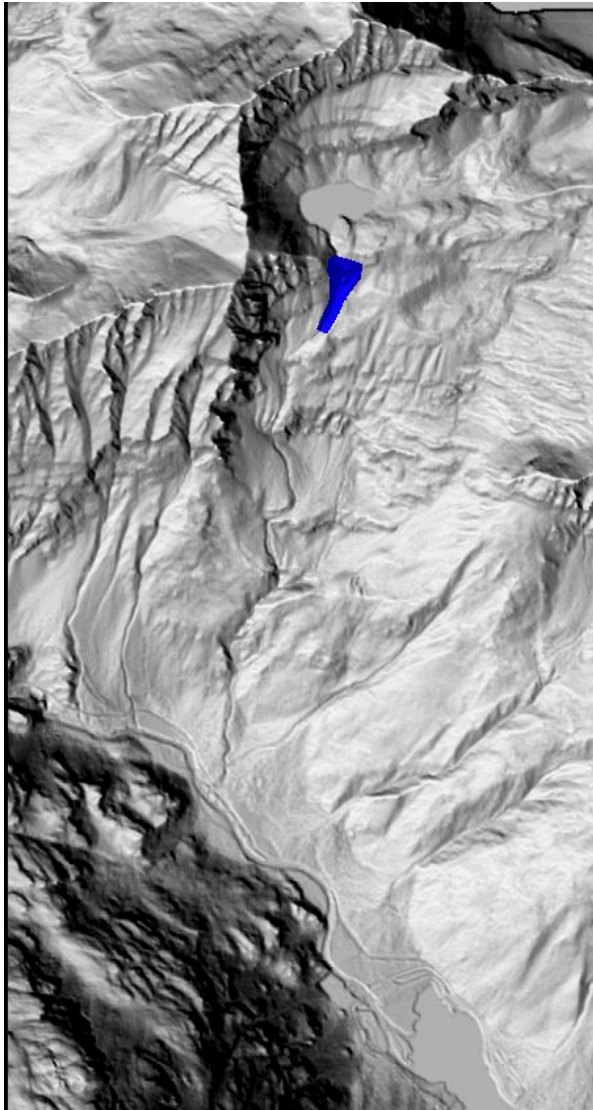
SNOWCOVER MENU							
<i>altitude</i>		<i>delta d</i>	<i>T.</i>	<i>delta t</i>	<i>water</i>	<i>delta w</i>	<i>Erosion depth</i>
<i>m</i>		<i>m/100m</i>	<i>°C</i>	<i>°C/100m</i>	<i>%</i>	<i>%/100</i>	<i>m</i>
2750		0.05	-1	0.40	1	0	2.5
<i>No snow steepness</i>	<i>Front splash</i>	<i>Yield stress</i>	<i>No snow altitude</i>	<i>Rel. density</i>	<i>Erosion density</i>	<i>Deposition density</i>	<i>Erosion mode</i>
<i>deg.</i>		<i>Pa</i>	<i>m s.l.m.</i>				
60	0	300	0	250	250	450	CONSTANT

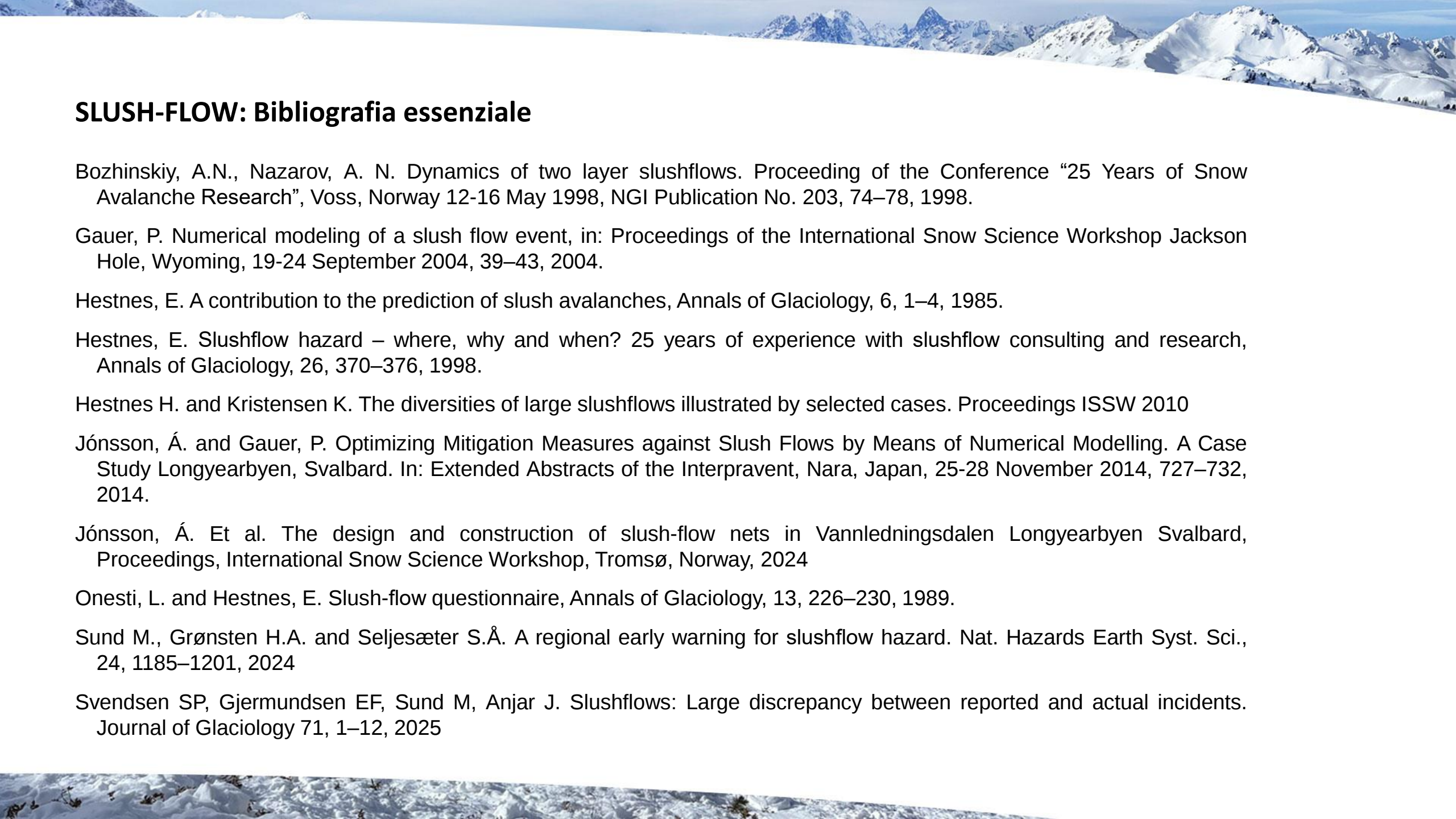
POWDER/WET MENU								
generate	mu wet	dry wet transition	Air temp [°]	cloud drag	cliff factor	turbul air entr	Enable turb	beta powder
%		mm						
3	0.05	2.0	-1.00	-	-	-	-	-



MODELLAZIONE EVENTO TIPO SLUSH-FLOW

Modello – RAMMS::Extended





SLUSH-FLOW: Bibliografia essenziale

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